

Surface plasmon polaritons on soft-boundary graphene nanoribbons and their application in switching/demultiplexing

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A graphene sheet gated with a ridged ground plane, creating a soft-boundary graphene nanoribbon, is considered. By adjusting the ridge parameters and bias voltage a channel can be created on the graphene which can guide transverse magnetic surface plasmon polaritons. Two types of modes are found; fundamental and higher-order modes with no apparent cutoff frequency and with energy distributed over the created channel, and edge modes with energy concentrated at the softboundary edge. Dispersion curves, electric near-field patterns, and current distributions of these modes are determined. Since the location where energy is concentrated in the edge modes can be easily controlled electronically by the bias voltage and frequency, the edge-mode phenomena is used to propose a voltage controlled plasmonic switch and a plasmonic frequency demultiplexer. © 2013 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4822044]

Graphene is the first two dimensional atomic crystal available to researchers, and has been the subject of intense study concerning both its fabrication and applications.^{1–13} Electrical properties of graphene, as represented by a local conductivity, are studied in many papers.¹⁴⁻²³ It has been shown that the conductivity of graphene consists of interband and intraband contributions whose imaginary parts have different signs. Assuming an $e^{i\omega t}$ time convention, at lower frequencies and lower temperatures the intraband term with negative imaginary part dominates the conductivity, otherwise the conductivity has a positive imaginary part due to the interband contribution. Furthermore, it has been shown that a graphene sheet can support a single TM surface plasmon polariton, and only in the regime where the conductivity has negative imaginary part.^{16,24} Likewise, when conductivity has a positive imaginary part only a TE mode can propagate. However, TE modes are very loosely confined to the graphene surface and are not considered further here.

The conductivity of graphene can be controlled by its carrier density, which can be varied by an electrostatic or magnetostatic bias, and/or chemical doping. This fact is used in Ref. 25 to implement a graphene based plasmonic switch. Recently, it has been proposed to use a perturbed ground plane as depicted in Fig. 1 in order to obtain different conductivities on the graphene, near and far from the ridge, by the use of a single bias voltage,²⁶ thereby creating an surface plasmon polariton (SPP) propagation channel parallel to the ridge. In Ref. 26 the ground plane ridge was assumed to form a conductivity profile with sharp features, i.e., to effectively form a hard-boundary (HB) graphene nanoribbon (GNR) wherein $\text{Im}(\sigma) < 0$ for |x| < W and $\text{Im}(\sigma) > 0$ for |x| > W, where 2 W is the ridge width and σ is assumed to be constant in each region. To remove the HB assumption, in Ref. 27 we studied the role of geometry and bias on forming the desired channel. In that work, rather than assuming a piece-wise constant conductivity, we determined the actual conductivity profile $\sigma(x)$ by finding the electrostatic charge distribution $\rho(x)$ on the graphene sheet from Laplace's equation, leading to the chemical potential $\mu_{c}(x)$ and the conductivity via the Kubo formula. It was shown that the ridged structure does indeed allow for the formation of a channel in the vicinity of the ridge for SPP propagation using a single bias, but that the resulting boundary has, as expected, a softened profile (i.e., a soft boundary (SB)) wherein the conductivity is not constant. The work²⁷ was concerned with the properties of the soft boundary and resulting channel, and the current distribution of the fundamental SPP mode. In this work we consider the various other modes that can propagate along the SB channel, including higher-order modes and edge modes. In particular, we show that unlike the HB case, for a soft boundary the higher-order modes have no apparent low-frequency/long-wavelength cutoff, although as frequency is lowered modal energy tends to spread out laterally along the effectively wider channel. We also show that lowloss edge modes can propagate for which the location where energy is concentrated can be controlled electronically. We then consider two applications of the structure, as a plasmonic voltage-controlled switch and a frequency demultiplexer.

Fig. 2 shows the conductivity profile $\sigma(x)$ of the graphene sheet for a representative set of geometrical and



FIG. 1. Graphene sheet gated with a ridged, perfect electrically-conducting (PEC) ground plane for the electrostatic bias, forming a soft-boundary graphene nanoribbon. The red area depicts the SPP channel having $Im(\sigma(x)) < 0$, and the blue area depicts the region where $Im(\sigma(x)) > 0$ and SPP propagation is prohibited.

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FIG. 2. Conductivity distribution on the graphene sheet. The red and the blue regions on the graphene indicate negative and positive $Im(\sigma)$, respectively.

electrical parameters; the SPP channel terminates where $\text{Im}(\sigma)$ becomes positive. The slope of the conductivity in the vicinity of the soft boundary can be adjusted by the ridge parameters.²⁷ Some other examples of SPP waveguide structures are Refs. 29 and 30. Throughout this work, the parameters of Fig. 1 are set as a = 25 nm, $b = 1 \mu \text{m}$, $V_0 = 20 \text{ V}$, and W = 25 nm. The mathematical formulation and numerical procedure are given in the supporting information.

SPP modes for the geometry in Fig. 1 are calculated by a rigorous electromagnetic analysis based on an electric-field integral equation (see Ref. 27 and supplementary materi als^{28}). Figure 3 shows the dispersion curves of the first three soft boundary modes. Also shown are the first four modes of a suspended³¹ graphene nanoribbon with width 50 nm and the same conductivity as for the SB modes for |x| < W, with $\sigma = 0$ for |x| > W. These modes are marked as HB modes, and are the usual GNR modes. As discussed in several papers,^{32,33} for the HB GNR the first two modes (called edge modes since energy is concentrated at the graphene edge, similar to that found for a graphene half-space) asymptotically merge to the edge mode of a semi-infinite graphene sheet. 33,34 The other higher order modes of the HB GNR become asymptotic to the single TM SPP mode²¹ that can propagate on an infinite graphene sheet. This HB behavior is shown in Fig. 3, where we also show that, unlike the HB case, for the soft boundary all modes become asymptotic to the infinite sheet SPP. In this regard, SB modes of the geometry are analogous to the sufficiently-higher-order modes (modes 3,4,.) of the HB GNR.

Figure 3 shows that there is no apparent cut off frequency for the SB modes. This is because, unlike a HB GNR with fixed width, as frequency decreases the effective width of the SB channel increases (i.e., the effect of the ridge perturbation which creates the propagation channel on the graphene sheet extends further away from the ridge as frequency is lowered). To clarify this, Fig. 4 shows the current, conductivity and field distribution of the first SB mode. Fig. 4(a) shows the normalized real part of the longitudinal current, Re(J_z), and the imaginary part of the conductivity, Im(σ), as a function of x. Fig. 4(b) shows the normalized magnitude of the longitudinal electric field $|E_z|$ in the transverse coordinate (x - y). Here we define an effective width for the channel (W_{eff}) as the width of the channel on the graphene sheet where Im($\sigma(x)$) < 0, which occurs in the



FIG. 3. Modal dispersion curves for the SB case (blue). For convenience, the SPP for an infinite graphene sheet (at $\mu_c = 0.239 \text{ eV}$) is also shown (red), as well as the modes of a HB GNR (black) with the same conductivity as the SB case for |x| < W (and $\sigma = 0$ for |x| > W).



FIG. 4. Re $(J_z(x))$ and $|E_z(x)|$ distributions of the first SB mode (1' in Fig. 3) at four different frequencies. The conductivity profile (Im (σ)) is also shown.

vicinity of the ridge (since only in this region can SPPs propagate). It is evident from Fig. 4 that $W_{\rm eff}$ increases as frequency decreases and therefore there is no cut off frequency for SB modes as exists for HB GNR modes (and, more generally, for all waveguides of fixed transverse dimensions), which is an important distinction between the SB and HB cases. Quantitatively, $W_{\rm eff}/W$ is 21.13, 8.97, 5.4, and 3.3 at 25, 40, 55, and 75 THz, respectively. The current distribution for SB modes is similar to those of HB GNR modes in the region |x| < W. Outside of this region the current vanishes after a few oscillations. These oscillations resemble the field distribution in the cladding of an optical fiber with graded index cladding.^{35,36} Since $\text{Im}(\sigma) > 0$ in the region $|x| > W_{\text{eff}}$, the current (and therefore the mode) is forced to be limited to the $|x| < W_{\rm eff}$ region. However, this is not a necessary condition for mode confinement (although it is sufficient). In Ref. 27 we show that even when $Im(\sigma) < 0$ everywhere on the graphene sheet (e.g., at low frequency and higher temperature) it is still possible to have modes confined near the ridge. In fact, the confinement condition is that the conductivity boundaries are sharp enough so that the current concentrates in the vicinity of the ridge.

The current and field distributions for the second and third SB modes are provided in the supporting information. Further higher order SB modes are not as important since they are very lossy.

As with a HB GNR, there are two degenerate edge modes for the geometry in Fig. 1, as considered in Fig. 5. These two even and odd edge modes propagate along edges of the created channel (i.e., in the region where $Im(\sigma)$ changes sign). As Fig. 5 shows, edge modes are slower and



FIG. 5. Dispersion curves of the geometry of Fig. 1 showing the previouslydiscussed bulk-like SB modes, and edge modes. There is no apparent cut off frequency for SB bulk modes. The edge modes are slower waves than the SB bulk modes.

less dispersive than the previously-discussed SB bulk-like (since current spreads out over the bulk of the created channel) modes. Therefore, at lower frequencies where the boundary is softer, these modes become more important since they are much slower than other SB modes. Fig. 6 shows the current and field distributions of the even edge mode for four different frequencies. Obviously, the even and odd classification can be interchanged by the left and right edge modes.^{32,33} The SB edge modes have two important properties: First, they are fairly low-loss and slow, and therefore more tightly confined to the graphene surface then the bulk SB modes (which, nevertheless, are fairly tightly confined to the graphene surface). Second, their physical location relative to the ridge varies with the applied bias voltage and frequency. The latter property makes the geometry useful for switching and demultiplexing applications, as proposed in the next section.

Since the effective width of the channel can be controlled by the bias voltage, the physical location where energy is concentrated for the edge modes can be easily controlled. One of the applications of this phenomena is a plasmonic voltage controlled switch as depicted in Fig. 7. By adjusting V_{control} in Fig. 7, the edge of the channel can be aligned with one of the receivers, and the edge mode can transfer energy from the transmitter to the desired receiver.



FIG. 6. $\text{Re}(J_z(x))$ and $|E_z(x)|$ distributions of the even edge mode at four different frequencies. The conductivity profile is also shown. As the frequency increases, the edge mode becomes closer to the step.



FIG. 7. A scheme to form a voltage-controlled plasmonic switch/demultiplexer. By adjusting V_{control} , the channel edge is aligned between the transmitter and the third receiver so that the edge mode can travel between them.

In Fig. 7, the ridge parameters and bias voltage are assumed to form the channel such that it's edge is aligned with receiver 3. On the other hand, it is evident from Fig. 6 that the channel width varies as frequency changes even with a fixed bias voltage. This suggests that we can design a plasmonic demultiplexer with the same geometry as shown in Fig. 7 with a fixed V_{control} . Then, e.g., lower frequencies can be transferred to receiver #1 and higher frequencies can be guided to, e.g., receiver #4. The characteristics of these plasmonic switches and demultiplexers can be determined by adjusting the distance between the receivers, ridge parameters, and the bias voltage range.

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Supporting information

The carrier density distribution of Fig. 1 is [IOP]

$$\frac{\rho(x)}{\varepsilon_0 V_0} = \begin{cases} \frac{1}{a} & |x| < W\\ \frac{1}{b} + \sum_{n=1}^{\infty} \frac{n\pi}{b} C_n (-1)^n e^{-\frac{n\pi}{b}(|x|-W)} & |x| > W \end{cases}$$
(1)

where

$$C_n = -\frac{2b}{a} \left(\frac{1}{n\pi}\right)^2 \sin\left(n\pi\left(1-\frac{a}{b}\right)\right).$$
⁽²⁾

This leads to the chemical potential

$$\mu_c(x) = \frac{\hbar}{e} v_F \sqrt{\frac{\pi \rho(x)}{e}}$$
(3)

where $v_F = 9.546 \times 10^5$ m/s is the Fermi velocity. The chemical potential is then used in the Kubo formula to find the graphene conductivity distribution $\sigma(x)$, [?]

$$\sigma(x) = \frac{je^2}{\pi\hbar^2(\omega - j\Gamma)} \int_0^\infty \varepsilon \left(\frac{\partial f_d(\varepsilon, x)}{\partial \varepsilon} - \frac{\partial f_d(-\varepsilon, x)}{\partial \varepsilon}\right) d\varepsilon - \frac{je^2(\omega - j\Gamma)}{\pi\hbar^2} \int_0^\infty \frac{f_d(-\varepsilon, x) - f_d(\varepsilon, x)}{(\omega - j\Gamma)^2 - 4(\varepsilon/\hbar)^2} d\varepsilon,$$
(4)

where is the charge of an electron, \hbar is the reduced Plank's constant, $f_d(\varepsilon, x) = \left(exp\left(\frac{\varepsilon-\mu_c(x)}{k_BT}\right)+1\right)^{-1}$ is the Fermi-Dirac distribution, k_B is the Boltzmann's constant, and $\Gamma = 10^{13}$ 1/s is the phenomenological scattering rate.

The eigenmodes of the structure are found starting with the Ohm's law

$$\mathbf{J}(x,\beta_z) = \sigma(x) \mathbf{E}(x,0,\beta_z), \qquad (5)$$

where the Fourier transform pair is defined as

$$\mathbf{E}(x, y, \beta_z) = \int_{-\infty}^{\infty} \mathbf{E}(x, y, z) e^{-j\beta_z z} dz$$
(6)

$$\mathbf{E}(x, y, z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \mathbf{E}(x, y, \beta_z) e^{j\beta_z z} d\beta_z.$$
(7)

Current and electric field are related as

$$\mathbf{E}(x, y, \beta_z) = \left(k_0^2 + \nabla_{\beta_z} \nabla_{\beta_z}\right)$$
(8)

$$\int_{x'} g\left(x, y, x', \beta_z\right) \frac{\mathbf{J}\left(x', \beta_z\right)}{j\omega\varepsilon_0} dx$$

where $\nabla_{\beta_z} = \frac{d}{dx}\hat{\mathbf{x}} + \frac{d}{dy}\hat{\mathbf{y}} + j\beta_z\hat{\mathbf{x}}$ and the Green's function is

$$g(x, y, x', \beta_z) = \frac{1}{2\pi} K_0 \left(\sqrt{\beta_z^2 - k_0^2} \sqrt{(x - x')^2 + y^2} \right), \tag{9}$$

 $K_0(x)$ being the zero order modified Bessel function of the first kind.

Equations (5) and (8) form an integral equation whose null space gives the eigenmodes of the structure (i.e. different β_z and their associated currents). We have used collocation method to solve the integral equations. The pulse function collocation method is used to solve the integral equation, with point matching at the center of the pulses. The eigencurrents in Figs. 4 and 6 are normalized so that the 2-norm of the eigen current vector (consists of transverse and longitudinal components) is unity $\left(\int \left(|J_x(x)|^2 + |J_z(x)|^2\right) dx = 1.\right)$ After finding the currents associated with the modes, 8 is used to find the filed distributions

$$E_{x}(x,y) = \frac{k_{0}^{2}}{2\pi j\omega\varepsilon_{0}} \int_{x'} K_{0}(\alpha) J_{x}(x') dx' + \frac{1}{2\pi j\omega\varepsilon_{0}} \int_{x'} \left\{ \frac{\partial^{2}}{\partial x^{2}} \left[K_{0}(\alpha) \right] J_{x}(x') + j\beta \frac{\partial}{\partial x} \left[K_{0}(\alpha) \right] J_{z}(x') \right\} dx'$$

$$(10)$$

$$E_{y}(x,y) = \frac{1}{2\pi j\omega\varepsilon_{0}} \frac{\partial}{\partial y} \int_{x'} \left\{ \frac{\partial}{\partial x} \left[K_{0}(\alpha) \right] J_{x}(x') + j\beta K_{0}(\alpha) J_{z}(x') \right\} dx'$$
(11)

$$E_{z}(x,y) = \frac{k_{0}^{2}}{2\pi j\omega\varepsilon_{0}} \int_{x'} K_{0}(\alpha) J_{z}(x') dx' + \frac{1}{2\pi j\omega\varepsilon_{0}} \int_{x'} \left\{ j\beta \frac{\partial}{\partial x} \left[K_{0}(\alpha) \right] J_{x}(x') - \beta^{2} K_{0}(\alpha) J_{z}(x') \right\} dx' \quad (12)$$

in which

$$\alpha = \sqrt{q_z^2 - k^2} \sqrt{(x - x')^2 + y^2}.$$
(13)

The currents $(\text{Re}(J_z(x)))$ and field distributions $(|E_z^2(x,y)|)$ associated with the second and third SB modes (2'and 3'in Fig. 6) at different frequencies are given in Figs. 8 and 9, respectively.

Two assumptions are made in the calculation of the surface modes. The conductivity distribution based on the electrostatic charge distribution is assumed to be only slightly perturbed by the modal fields, i.e., $\frac{\nabla \cdot \mathbf{J}}{j\omega} \ll \rho$ where ρ is the static charge density and \mathbf{J} is the modal current density. The second assumption is that the the ground plane (and its ridge) are far enough from the surface that the ground plane does not interact with the (tightly-confined) modal fields. The parameters of the geometry is chosen so that these assumptions are both valid.



Figure 1: $Re(J_z(x))$ and $|E_z(x)|$ distributions of the second SB mode (2' in Fig. 3) at four different frequencies.



Figure 2: $Re(J_z(x))$ and $|E_z(x)|$ distributions of the third SB mode (3' in Fig. 3) at four different frequencies.